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Optical and electrical properties of nanostructured metallic electrical contacts

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## Abstract

PAPER

We study the optical and electrical properties of silver films with a graded thickness obtained through metallic evaporation in vacuum on a tilted substrate to evaluate their use as semitransparent electrical contacts. We measure their ellipsometric coefficients, optical transmissions and electrical conductivity for different widths, and we employ an efficient recursive method to calculate their macroscopic dielectric function, their optical properties and their microscopic electric fields. The topology of very thin films corresponds to disconnected islands, while very wide films are simply connected. For intermediate widths the film becomes semicontinuous, multiply connected, and its microscopic electric field develops hotspots at optical resonances which appear near the percolation threshold of the conducting phase, yielding large ohmic losses that increase the absorptance above that of a corresponding homogeneous film. Optimizing the thickness of the film to maximize its transmittance above the percolation threshold of the conductive phase we obtained a film with transmittance T = 0.41 and a sheet resistance  $R_s^{max} \approx 2.7 \Omega$ . We also analyze the observed emission frequency shift of porous silicon electroluminescent devices when Ag films are used as solid electrical contacts in replacement of electrolytic ones.

# 1. Introduction

Transparent electric contacts are needed in a widespread variety of optoelectronic applications. Materials such as coinable metals are very good electrical conductors when compared to the conductive polymers or semiconductor materials often used for those applications [1], but unfortunately, they are opaque. Organic conductive materials and doped metallic oxides have been considered a good compromise, behaving as conductors at low frequency and as dielectrics at optical frequencies [1]. Nonetheless, the properties of these semiconductor materials are defined by their chemical composition and their doping. Thus, tuning the threshold frequency at which they change behavior from conductor to dielectric is difficult. An alternative for the design of semitransparent electrical contacts is the use of nanostructured metallic-dielectric composites. Extraordinary optical transmission [2] in perforated metallic films with nanoperforations has been explained in terms of bulk and surface plasmons in nanostructured films [3] and is promising for the control of optical properties [4]. These systems, are composed of a metallic and a dielectric phase; one of them may be described as an array of nanometric inclusions with a given geometry. Material composition, geometry, and order affect the optical properties of the system [5, 6]. Fabrication of nanostructured films with ordered patterns designed to tune optical properties in the visible (VIS) range requires high resolution lithography, employing interferometry of electronic beams [7, 8] or similar techniques. A relative simple alternative is to use random composite films [9]. Unlike the metallic oxides, this kind of semitransparent contacts do not require high temperatures, are flexible, might possess low enough surface roughness for the optical range, and have a relatively low cost of production.

It is well known that the optical transmission [9] as well as the electrical resistivity [10] of uniform metallic thin films increase as the films becomes thinner. However, the reduction of the thickness of a film usually modifies

its morphology leading to inhomogeneities. A thin enough film is made of separate *islands* [11] and is therefore non-conducting. Near but above the percolation threshold, while the conductive phase is connected, there appear optical resonances at which the transmittance is suppressed due to the power dissipated as Joule heat [12]. In the present work, we employ a computationally efficient recursive formalism for the calculation of an effective dielectric response of nanostructured films when the length-scale of the inhomogeneities of the film are much smaller than the wavelength, thus neglecting retardation [5, 6, 13]. This non-retarded recursive method (RM) is applicable [14] to nano-textured inhomogeneities with scales up to one order of magnitude below the nominal wavelength. Analyzing the optical and electrical properties of semicontinuous Ag films with a graded thickness we have searched for an optimum film, with an adequate conductivity in the low frequency range and a relatively high transmittance in the VIS.

We also study Ag electrical contacts on porous silicon (PS) electro-luminescent devices (ELD). It is known [15] that in metal/PS/cSi junctions under a bias voltage the injected carriers may recombine. Due to the quantum confinement within the thin Si regions in PS, direct radiative transitions with an energy larger than the bulk indirect gap become permitted, leading to electro-luminescence (EL) in the VIS range of the spectrum. Photo luminescence (PL) may also be observed if the sample is irradiated by ultraviolet (UV) light. A relation between the PL spectra with the porosity p and the morphology of PS was proposed by Bessaí et al [16] yielding a maximum emission at at 680 nm with p = 0.8. Under similar preparation conditions, the PL and EL spectra are expected to be similar [17]. EL spectra from PS excited through an electrolytic contact [18] have been characterized as a function of the excitation potential and electric current, allowing the control of the emission spectra through the preparation condition. However, it has been found that the EL spectra of similarly prepared PS films samples differ when they are excited through different solid contacts. For PS with an expected porosity around 80% over p doped Si with Au vacuum evaporated contacts (Au/PS/p-Si/Al), a peak emission was obtained at 680 [19]. Similarly for an ITO contact [19] or for an Al contact and an *n* doped substrate (Al/PS/*n*-Si/Al) [17]. Nevertheless, for an Au contact prepared by sputtering (Au/PS/p-Si/Al) the EL peak shifts to 560 nm [20]. Other shifts have been reported for contacts made through the co-evaporation of Au and Ga or Sn (530 nm), Au and In (455 nm), and Au and Sb (700 nm) [21]. In the above cases the intensity of the EL signal was strongly suppressed.

In this paper we also explore experimentally and theoretically the spectral shift and the intensity suppression of the EL signal when an electrolytic contact over an PS-ELD is replaced by a solid Ag contact.

The paper is organized as follows: In section 2 we present our method for fabricating Ag films with variable thickness in only one evaporation step (section 2.1), and we discuss our procedures for measuring the transmittance, ellipsometric coefficients and resistance (section 2.2). In section 3 we discuss our model for the semicontinuous film and we describe our computational procedures. In section 4 we obtain theoretical results from the RM for the ellipsometric coefficients (section 4.1), the electrical properties (section 4.2), and the transmittance (section 4.3) of semicontinuous films. As an application, in section 5 we fabricate an optimally tuned solid transparent electrical contact (section 5.1) and we propose an explanation for the spectral shift and the suppression of the observed emission of a PS-ELD (section 5.2). We devote section 6 to conclusions.

## 2. Experimental

In this section we describe the experimental setup employed to determine the optimal thickness of thin metallic films by fabricating samples with a graded thickness and measuring their optical transmittance, ellipsometric coefficients, and four-point electrical resistance. The optimal thickness would be the one that maximizes the transmittance and minimizes the resistance.

## 2.1. Sample preparation

Figure 1 displays our setup for growing film samples with a graded thickness (*h*), adapted from a coinable-metal vacuum evaporation technique [22, 23]. The sample is obtained by isotropic thermal evaporation of Ag through a solid angle  $\gamma \pi$  determined by the aperture of a conical molybdenum crucible whose walls screen the lower part of a vacuum bell device. On a surface element  $d\vec{s}$  at position  $\vec{r}$  on a glass slide, the deposited mass dm is given by  $-m\hat{r} \cdot d\vec{s} / (\gamma \pi r^2)$  where *m* is the total Ag mass vaporized. A nominal width *h* may be obtained by dividing the mass per unit area of the film by the bulk mass density of Ag. The actual density may be smaller and the actual width larger due to texture of the film. Due to the inclination  $\alpha$  of the slide with respect to the horizontal, the deposited film is thicker on the side that is closer to the source, at a height  $y_0$  above the crucible, and thinner on the opposite side. Thus, we can prepare samples with variable thickness within a range that depends on the geometrical parameters of the experimental setup. We show below results for two samples, both prepared with  $\gamma = 1.1$ , sample S1 with  $y_0 = 10 \text{ cm}$ ,  $\alpha = 32^\circ$ , m = 16.5 mg and sample S2 with  $y_0 = 9.7 \text{ cm}$ ,  $\alpha = 42^\circ$ , and m = 8.25 mg. The inset of figure 1 shows the thickness *h* as a function of position  $\ell$  along the sample S1.



**Figure 1.** Experimental setup for the growth of films with a graded thickness using a coinable-metal vacuum evaporation technique. A molybdenum crucible with an aperture that spans a solid angle  $\gamma \pi$  supports a small piece of Ag wire that is melted and vaporized by contact with an electrical heating device (not shown). The sample with variable thickness (dark gray) is grown on a glass slide (light gray) tilted an angle  $\alpha$ . We indicate a differential element of surface  $d\vec{s} = -ds \hat{n}$  at position  $\vec{r}$ , and the height  $y_0$  of the lower edge of the slide. Inset: nominal height *h* versus position  $\ell$  along the sample calculated from  $\alpha$ ,  $y_0$ , *m* and  $\gamma$  for sample S1.

#### 2.2. Optical and electrical properties

We measured and averaged the optical normal-incidence transmittance along three parallel equispaced lines running longitudinally through the sample in the gradient direction, using (a) a 650 nm diode laser with a spot of diameter 1.5 mm, and (b) an Ocean Optics UV-NIS-NIR source through an optical fiber. In both cases we measured the intensity of the transmitted light at  $\Delta \ell = 5$  mm intervals. We used a clean glass slide as a reference. For (a) we used a detector based on a photo-diode BPW20RF and in (b) the data were collected from a USB spectrometer and we employed the *Spectrasuite* software. We also determined the sheet resistance  $R_s$  over the same places using a four-point technique [22, 24].

We measured the ellipsometric parameters of the sample  $\psi$  and  $\delta$ , defined through

$$\frac{r_p}{r_s} = \exp(i\delta)\tan(\psi),\tag{1}$$

where  $r_p$  and  $r_s$  are the reflection coefficients for p and s polarization, respectively, with a Rudoph Research type 43702-200E ellipsometer in the null field mode [25]. We fixed the incidence angle  $\theta$ , we put a linear polarizer and a quarter wave plate across the incident beam oriented at angles P and C with respect to the plane of incidence, respectively, and a linear analyzer across the reflected beam at an angle A. We set  $C = \pi/4$  and found  $\delta = 2P + \pi/2$ , and  $\psi = A$  for different film thicknesses and wavelengths, where we choose P and A to minimize the intensity of the outgoing beam.

## 3. Model

For very thin films of coinable metals an *island* morphology type has been reported [4, 10]. As the film grows the islands eventually connect among themselves, leading to a semicontinuous film textured in the nanometric scale [10, 11, 26]. For thickness smaller than a couple dozen nanometers, the air interstices among the islands may sustain resonant excitations that significantly modify the optical [5, 6] and electrical [27] properties. As we move along our graded sample towards its thick edge those islands become more connected and for very thick films they merge into a continuous film. Figure 2 shows schematically the proposed morphology. Our model consists of an ensemble of periodically repeated unit cells, each of which contains a large enough number of penetrable disks of radius *a* and height  $h_d$  occupying random uncorrelated positions. The ensemble is characterized by the filling fraction *f*, i.e. the fraction of the area covered by the metal, and the amount of metal deposited per unit area, which in turn is characterized by the nominal height *h*. We employed the RM to calculate the macroscopic dielectric function  $e^M$  of the composite [5, 6, 14] using the *Photonic* package [13]. The filling fraction *f* may be adjusted in the model by varying the radius *a* of the disks and the height  $h_d$  is related to *f* through  $h_d = h/f$ .





## 4. Results

## 4.1. Ellipsometric coefficients

We measured the ellipsometric coefficients at a fixed incidence angle  $\theta = 69^\circ$ . We measured  $\delta$  and  $\psi$  at ten different positions  $\ell$  along sample S1 and five wavelenghts  $\lambda = 405, 451, 492, 546$  and 580 nm. In the left panel of figure 3 we show our results for three of those (we omitted two to avoid cluttering the figure). Each point in figure 3 corresponds to a different thickness  $h(\psi \text{ increases with } h)$ . For thick films (above 20 nm) experiment agrees roughly with the values of  $\psi$  and  $\delta$  calculated for a locally homogeneous film of width h with a dielectric function  $\epsilon_{Ag}$  taken from [28] (commonly used for studying optical properties of Ag composites at frequencies in UV-VIS-NIR range) and deposited over glass, with dielectric response obtained from [29], but they don't agree for thinner films (h < 20 nm) for which the film inhomogeneities lead to a strong dependence of the optical response with the film morphology. For each value of  $\ell$  and h we used our model (section 3) to obtain the macroscopic response of the film and identifying the width of the film with the height  $h_d$  of the disks we calculated the ellipsometric coefficients. To this end we averaged our results over a thousand realizations of our ensemble with thirty disks randomly situated within a square unit cell. We have verified convergence of the results. Our model has only one parameter, namely, the radius a of the disks, and it is adjusted for each value of  $\ell$  with corresponding nominal width h to best reproduce the ellipsometric measurements at the five wavelengths mentioned above. Figure 2 displays the fitted values of  $h_d$  at the ten positions  $\ell$  for which we measured  $\delta$  and  $\psi$ . It also displays the resulting filling fraction f as a function of the nominal height h, together with an analytical fit, for which we chose the form

$$f = \frac{\mu h}{\sqrt{1 + (\mu h)^2}},\tag{2}$$

as it is linear for thin films and saturates at f = 1 for very thick ones. We obtained the parameter  $\mu = 0.11$  nm<sup>-1</sup>.

The left panel of figure 3 shows that results of our RM calculation agree with experiment for most of the film thicknesses explored. In contrast, the effective medium models of Maxwell–Garnett (MG) and Bruggeman (B) [30] differ strongly, as shown in the right panel of figure 3 corresponding to  $\lambda = 580$  nm. Thus, our model system and the RM computational procedure are much better suited for the calculation of the effects of the nanometric texture on optical properties of very thin films. It has been reported [10, 11] that optical properties of inhomogeneous films (such as semicontinuous films of coinable metals) differ from those of homogeneous films. However, to our knowledge, this is the first time that semicontinuous Ag films are analyzed and that the differences between homogeneous and inhomogeneous films are calculated and compared to those measured on a single sample consisting of a film with a graded thickness. This kind of analysis allows correlation of the parameters needed to design and manufacture semicontinuous films with optimal parameters.





#### 4.2. Resistance

In figure 4 we show our measurements of the sheet resistance  $R_s$  at various positions  $\ell$  on sample S2, prepared with a larger angle  $\alpha$  and a smaller mass *m* than sample S1, so that for each position  $\ell$  the corresponding film is thinner. We also show the filling fraction calculated for each  $\ell$  using equation (2) (fitted to the ellipsometric parameters of sample S1) and using the nominal height *h* as a function of  $\ell$  as described in section 2.1. Notice that the resistance increases very fast as  $\ell$  increases, the film becomes thinner, and the filling fraction of the metal diminishes, indicative of the approach to a percolation transition at  $f_c \approx 0.7$  where the resistance would diverge (we couldn't measure the resistance for filling fractions smaller than 0.74). In sample S2 this region corresponds roughly to the center of the sample, whereas in sample S1 it is too close to one of its edges, difficulting its measurement.

From the filling fraction f and the nominal height h we obtained the height  $h_d$  of our model disks. This allows us to calculate the resistivity

$$\rho^{M} = \frac{4\pi}{\lim_{\omega \to 0} \omega \operatorname{Im}\{\epsilon^{M}(\omega)\}},\tag{3}$$

and the sheet resistance  $R_s = \rho^M / h_d$  using the RM model. To that end, we extrapolate the dielectric function of the metallic phase towards low frequencies using the Drude model

$$\tau_{\rm Ag} = 1 - \frac{\omega_p^2}{\omega^2 + i\omega\gamma}.$$
 (4)

with parameters  $\hbar \gamma = 0.021 \text{ eV} [4]$ ,  $\hbar \omega_p = 8.51 \text{ eV}$ , which correspond to the resistivity  $\rho_{Ag} = 2.16 \times 10^{-6} \Omega \text{cm}$ which we measured for the same Ag wire from which the samples were prepared.

The theoretical results are displayed in figure 4. Notice that they also increase rapidly as  $\ell$  increases, though not as rapidly as experiment. We recall that the geometrical percolation threshold for penetrable disks is  $f_c = 0.676$  [31] and that our calculations are done on a system made up of a periodically repeated finite random unit cell so that we expect finite size effects to wash away the percolation transition in our calculation. In the same figure we also include the sheet resistance  $\rho_{Ag}/h$  of a continuous film. Its behavior is qualitatively different from both experiment and our calculation. Of course, for small  $\ell$  and high filling fractions both models coincide and agree with experiment.

#### 4.3. Transmittance

Figure 5 displays the transmittance *T* normalized to the transmittance  $T_s$  of the glass slide as function of position  $\ell$ , and thus, as a function of the filling fraction *f*, measured at  $\lambda = 650$  nm for sample S2. We also show the transmittance calculated with the RM model and the result for a homogeneous film.

As  $\ell$  increases and f decreases the experimental transmittance increases up to a local maximum T = 0.41 corresponding to a filling fraction  $f_{\text{max}} \approx 0.84$  for which the film is conducting as it lies above the percolation threshold  $f_c \approx 0.7$  displayed in figure 4. Afterwards, T diminishes and reaches a local minimum T = 0.29 at  $f_{\text{min}} \approx 0.74 \gtrsim f_c$ . As the filling fraction diminishes further, the transmittance of the film increases again, but for  $f < f_c$  the film is no longer conducting. The RM calculation does not show the maximum and minimum discussed above, but displays a similar inflection, and it follows the experimental results much more closely than the calculation for a homogeneous film.

The optical properties close to the percolation threshold depend strongly on the morphology and on the wavelength. In this region field fluctuations are very intense and localized optical resonances known as *hotspots* 



**Figure 4.** Sheet resistance  $R_s$  measured for sample S2 (crosses with error bars) as a function of position  $\ell$  along the sample (top panel). We also show the results  $\rho^M/h_d$  calculated with the RM theory for the morphology illustrated in figure 2 (diamonds with lines) and the results  $\rho_{Ag}/h$  for a locally homogeneous Ag film (dashed line). In the bottom panel we include the calculated filling fraction f as a function of position  $\ell$ .



occur. To illustrate the hotspots, in figure 6 we show the microscopic field obtained through a recursive procedure based in the RM calculation of the response [13, 32]. We show the field for two different members of the random ensemble that models the morphology of the system and for three disk radii a = 0.11, 0.12, 0.13, corresponding to the averaged filling fractions  $f \approx 0.69, 0.75, 0.81$ , at a single wavelength  $\lambda = 650$  nm. Figure 6(c) displays hotspots in the interstice between two nearby particles (bottom left) and between three particles (bottom right), in which  $|\vec{E}|$  is approximately 2 orders of magnitude larger than its mean value. Similar hotspots appear at different positions for different wavelengths and for different filling fractions, as illustrated by the other panels of the figure. Figure 6(b) shows four different hotspots for a slightly smaller *f*. With *f* even smaller figure 6(a) shows no hotspots. But, another member of the ensemble ensemble with the same *f* displays several as exemplified by figure 6(d). The set of hotspots for that member also change position and intensity as *f* grows (figures 6(e) and (f)). There are well known results on the scaling of the localized states for disordered random [33, 34] and fractal [35, 36] systems. These localized states have found applications due to the corresponding enhancement in linear and nonlinear signals. For example, SERS and KERS enhancements of 1 to 2 dozen orders of magnitude have been reported [37, 38].

The presence of hotspots in the microscopic field for filling fractions around the percolation threshold is responsible for an increased energy absorption within the conducting film, and thus to the decrease in the transmittance T as compared to that of a homogeneous film, as seen in figure 5 for  $f < f_{max}$ . This energy absorption corresponds to Joule heat that is related to the imaginary part of  $e^M$ . Figure 7 displays the real and imaginary parts



**Figure 6.** Absolute value |E| of the microscopic field normalized to that of the incident field  $|E_0|$  calculated with the RM model at  $\lambda = 650$  nm for two members (left and right columns) of the ensemble and for three different radii and average filling fractions a = 0.11,  $f \approx 0.69$  ((a) and (d)), a = 0.12,  $f \approx 0.75$  ((b) and (e)), and a = 0.13,  $f \approx 0.81$  ((c) and (f)).



**Figure 7.** Ensemble average of the imaginary part (top panel) and real part (bottom panel) of  $\epsilon^{-\alpha}$  calculated within the KM function of the filling fraction f and the wavelength  $\lambda$ .

of the ensemble average of  $\epsilon^M$  as a function of the filling fraction and of the wavelength. For  $f \leq 1$ ,  $h_d \approx h$ , Im  $\epsilon^M$  is relatively small and Re  $\epsilon^M < 0$ . Thus, the index of refraction  $n^M = \sqrt{\epsilon^M}$  is close to an imaginary number, the film is opaque and the field decays across it by a factor  $\exp(-h \operatorname{Im} n^M)$ . Therefore, as  $\ell$  increases and h decreases the transmittance T increases. As f decreases further, Re  $\epsilon^M$  becomes less negative and the field penetrates more into the film. Nevertheless, Im  $\epsilon^M$  also increases and reaches a maximum for  $f \approx 0.72$ , thus increasing the absorption and decreasing the transmittance. For even larger  $\ell$  and smaller f the film becomes dielectric and the transmittance increases again. This explains qualitatively the maximum and minimum transmittance observed in figure 5. The







corresponding inflection in the transmittance is reproduced by our numerical calculation, although not the actual maximum and minimum.

# 5. Applications

## 5.1. Optimization of semicontinuous Ag film

An optimal transparent electrical contact would have the highest possible transmittance and the lowest possible resistance. To choose the best combination of parameters we plot *T* as a function of  $R_s$  in figure 8, combining information from figures 4 and 5. It is clear that it is not useful to diminish the nominal width *h* of the film too much, as the transmittance stops increasing while the resistance does. Thus, an optimal choice would correspond to the maximum transmittance which corresponds to  $T/T_s = 0.41$ ,  $R = 2.7 \Omega$ ,  $\ell = 2 \text{ cm}$ , f = 0.84, h = 13.8 nm,  $h_d = 16.4 \text{ nm}$ .

#### 5.2. Electro-luminescence of PS with an Ag contact

We analyze light emitting devices (LED) made of porous silicon (PS) over which Ag is sputtered to form an electrical contact. We prepare the PS sample by anodizing a crystalline *p*-doped Si substrate with resistivity 0.5–1.0  $\Omega$  cm terminated in a (100) surface, using a well known procedure: [39] We immerse the Si crystal in an electrolytic solution of hydrofluoric acid, distilled water, and ethanol in proportions 1:1:2 and we apply a current with a density of 20 mA cm<sup>-2</sup> for a duration of 120 s [12] to obtain a sample with an expected porosity  $p \approx 80\%$ . We discard the electrolytic solution and clean the system with an ethanol bath.

If we use a diluted solution of potassium chloride as an electrolytic contact and apply a forward current with density 16 mA cm<sup>-2</sup> an electroluminescent signal is produced. We measured the normalized spectral emission with a Hitachi fluorimeter F2000 with blocked excitation source 25 s after turning the current on [40]. The results are displayed in figure 9.

It is well known that luminescence of PS [41] is due to the confinement of charge carriers within the pore walls, which introduces an uncertainty in the momentum that allows direct transitions that would be forbidden in bulk



**Figure 10.** Top panel: normalized photoluminiscence signal  $I_{PL}$  of porous silicon (PS) calculated as a function of porosity p and wavelength  $\lambda$  [39]. Bottom panel: product  $I_{PL}$  of top panel with  $T_i$  for a simulated composite PS and PS permeated with Ag.





Si [42]. Thus, the  $\lambda = 1130$  indirect gap of bulk Si gives rise to a direct electronic transition in PS that is shifted due to quantum confinement and corresponds to the emitted emission with wavelength  $\lambda = 680$  nm illustrated by the peak on the right of figure 9 corresponding to an electrolytic contact [21]. While the current flows, silicon oxide is progressively produced on the walls of the pores, increasing the confinement and producing a small blue shift of the maximum emission peak [39]. After the current had been applied for approximately 90 s the electroluminiscence of our sample was extinguished.

The electrical excitation of PS may also be realized with Schottky type metallic solid contacts [21]. An advantage of metallic contacts is that the electric current doesn't produce the chemical reactions that rapidly destroys the electroluminiscence when an electrolytic contact is employed, extending the life of the device. To produce a metallic contact, we use cathodic projection (sputtering) of Ag on a 0.2 cm<sup>2</sup> masked surface of a PS sample fabricated as described above. We chose the sputtering conditions (pressure, arc current, distance of Ag target to sample, deposition time) by first sputtering onto a glass sample and selecting those conditions that yielded a film with relative transmittance  $T/T_s \approx 0.2$ .

Figure 9 shows the electroluminiscence spectrum of our sample with a metallic contact excited by an electric current with density of 20 mA cm<sup>-2</sup>. Comparing this spectrum with that corresponding to the electrolytic contact,

we notice that it is strongly blue-shifted towards the central part of VIS spectra ( $\approx$ 550 nm), but that its intensity is about two orders of magnitude smaller.

To understand the shift of the maximum of the emission spectra from  $\lambda = 680$  for an electrolytic contact to  $\lambda = 550$  for an Ag contact, we obtained the emission spectra from the photo-luminescence (PL) spectra of Si nano-crystals and their size dependence [42]. The effects of confinement in the walls of PS have been related to the effects of confinement in nano-crystals and a relation between porosity and effective size has been proposed [16], as well as analytical expressions for the shift of the emission peak with respect to size [43]. If the sample is kept in air there is a further blue shift due to oxidation at the surface of the pores [20, 21]. Thus, we model the intrinsic PL spectrum of PS as a Gaussian of an appropriate width centered at the energy corresponding to the porosity, and we assume that the EL emission spectrum is similar to the PL one. In the top panel of figure 10 we show the resulting PL spectra as a function of both wavelength and porosity [39].

When using a solid contact, the light produced through EL is transmitted through the contact before being observed. Thus we expect that the observed EL signal should be given by the product of the emission, similar to the the PL spectrum, and the optical transmittance of the system PS/contact/air. We model the contact by assuming most of the metal infiltrates the pores. We used the RM method to calculate the macroscopic dielectric response of PS modeled as a random ensemble of empty cylinders within a crystalline Si host of porosity p [27], and we also use the RM method to calculate the macroscopic dielectric response of the contact modeled as a random ensemble of Ag cylinders within a filling fraction given by the porosity. We calculate the transmittance  $T_i$  of the system formed by PS covered with a filling of width d made up of Ag-infiltrated PS. In figure 10 we also show the product of the intrinsic PS luminescence signal with the transmittance  $T_i$  for d = 45 nm. Notice that the signal is suppressed about two orders of magnitude with respect to the PL spectrum and that it is becomes blue shifted and more intense as the porosity increases.

Finally, we assume that the porosity in our random sample is not fixed at the nominal value  $\bar{p} = 80\%$  expected from our preparation procedure, but has some fluctuations. We assume p is distributed as a Gaussian of width  $\sigma = 0.14$  around its average  $\bar{p}$  and. In figure 11 we show the corresponding EL spectra for different thicknesses d of the contact.

The curve for d = 0 corresponds to the absence of metal, and thus may be compared to the EL spectrum with a transparent electrolytic contact. It has a peak at 680 nm which agrees well with that in the right side of figure 9. The peak is slightly red shifted with respect to the nominal peak corresponding to  $p = \bar{p} = 0.8$  in the top panel of figure 10, as the direction of its ridge is closer to that of the *p* axis for lower frequencies.

On the other hand, the peaks of the curves corresponding to d = 25 nm and d = 45 nm are blue shifted to 590 nm and 570 nm and are suppressed about one and two orders of magnitude respectively. The reason for the shift and the height decrease of the peaks lies in the absorption within the contact, as illustrated in the top panel of figure 11, which shows that the macroscopic index of refraction of the contact is large and increases with wavelength, therefore yielding a stronger suppression at the red end of the spectrum. Thus, our model of a metallic contact that partially infiltrates the pores PS is able to explain blue shift and suppression of the EL spectra observed experimentally and illustrated by the curve on the left side of figure 9. On the other hand, we were unable to reproduce the experimental results using a metallic semicontinuous overlayer, as in the previous sections, as a contact. Our results are not very sensitive to the width  $\sigma$  of the porosity distribution, but we don't get a large enough shift in the limit  $\sigma \rightarrow 0$ .

# 6. Conclusions

We prepared Ag thin films with a height gradient by evaporation onto a tilted glass substrate. We performed ellipsometric measurements which showed than the films changed nature from locally homogeneous to semicontinuous and to an island morphology as their width diminished. We modeled the system as an ensemble of penetrable metallic cylinders occupying random uncorrelated positions, and we applied an efficient recursive formalism to obtain its macroscopic dielectric function. We fitted the ellipsometric measurements to relate the position along the sample film and the nominal height of the film to its actual height and its (area) filling fraction. We measured and analyzed the sheet resistance of the film was also measured and analyzed, and we obtained a deviation from that of a homogeneous film. As the film narrows, its transmittance reaches a maximum and then a minimum. We expect the inhomogeneities of the film to have a lengthscale smaller than the wavelength of light, so that scattering is small [44] and we characterized the film by a macroscopic effective permittivity [14]. Our model calculation of the dielectric response captured qualitatively the behavior of the transmittance and explained it in terms of plasmonic resonances within the film. For filling fractions around the percolation threshold the field may become very intense in very small hotspots that are responsible for an increased energy dissipation within the

film. We employed our results to optimize a film for use as a semitransparent contact. We also calculated the shift towards the blue and the decrease in the intensity of the electro-luminescence of porous silicon when a metallic semicontinuous contact that infiltrates the inhomogeneous pores is employed instead of an electrolytic one.

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